**ORIGINAL PAPER** 



# RKDG Methods with Multi-resolution WENO Limiters for Solving Steady-State Problems on Triangular Meshes

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# Abstract

In this paper, we design high-order Runge-Kutta discontinuous Galerkin (RKDG) methods with multi-resolution weighted essentially non-oscillatory (multi-resolution WENO) limiters to compute compressible steady-state problems on triangular meshes. A troubled cell indicator extended from structured meshes to unstructured meshes is constructed to identify triangular cells in which the application of the limiting procedures is required. In such troubled cells, the multi-resolution WENO limiting methods are used to the hierarchical  $L^2$  projection polynomial sequence of the DG solution. Through using the RKDG methods with multi-resolution WENO limiters, the optimal high-order accuracy can be gradually reduced to first-order in the triangular troubled cells, so that the shock wave oscillations can be well suppressed. In steadystate simulations on triangular meshes, the numerical residual converges to near machine zero. The proposed spatial reconstruction methods enhance the robustness of classical DG methods on triangular meshes. The good results of these RKDG methods with multi-resolution WENO limiters are verified by a series of two-dimensional steady-state problems.

Keywords RKDG method  $\cdot$  Steady-state problem  $\cdot$  Multi-resolution WENO limiter  $\cdot$  Triangular mesh  $\cdot$  Machine zero

# Mathematics Subject Classification 65M60 · 35L65

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## 1 Introduction

In this paper, we design high-order Runge-Kutta discontinuous Galerkin (RKDG) methods [8–10, 12] with multi-resolution WENO limiters [50] to compute the two-dimensional steady-state Euler equation

$$\begin{cases} f_x(u) + g_y(u) = 0, \\ u(x, y) = u_0(x, y) \end{cases}$$
(1)

on triangular meshes. This is a method to compute (1) by solving the two-dimensional unsteady Euler equation

$$\begin{cases} u_t + f_x(u) + g_y(u) = 0, \\ u(x, y, 0) = u_0(x, y). \end{cases}$$
(2)

We use high-order DG methods for the spatial discretization and the explicit and nonlinearly stable Runge-Kutta methods [13, 40] for the temporal discretization to make the numerical residuals converge to near machine zero. The main work is to construct a troubled cell indicator which is extended from structured meshes [51] to unstructured meshes, and apply it to identify triangular cells in which the application of the higher-order limiting procedures is required, and then use the DG methods with the multi-resolution WENO limiters [50] to compute two-dimensional steady-state problems on triangular meshes. The troubled cell indicator is needed to obtain steady state convergence to near machine zero.

When the numerical residual of the two-dimensional unsteady Euler equation (2) is near machine zero, the numerical solution of the two-dimensional steady-state Euler equation (1) is achieved. There will be strong discontinuities when solving (1) and (2). In the past, many high-resolution numerical schemes have been proposed, mainly using artificial viscosities [22, 23] or nonlinear limiters [19, 22, 41] to suppress the oscillations. Jameson et al. [21, 24] designed a third-order finite volume method with dissipation terms to simulate steady-state problems. But to accurately simulate strong shocks in the numerical simulation, they often needed to adjust some parameters in the artificial viscosity. In 1983, Harten [19] found that numerical schemes with limiters were very effective in simulating supersonic flow problems. However, when the total variation diminishing (TVD) limiters [34] were used, it was difficult for the numerical residuals to converge to near machine zero. In 1985, Yee et al. [44] proposed the implicit TVD schemes for the steady-state calculation. Two years later, Yee and Harten [43] proposed an implicit TVD scheme for hyperbolic conservation laws in curvilinear coordinates. The researchers found that the numerical residuals could not be reduced to machine zero when the classical WENO scheme [25] was used to compute the steady-state problems. In 2004, Serna and Marquina [37] designed a fifth-order accurate weighted power ENO method, which significantly improved the convergence of the numerical scheme. Three years later, Zhang and Shu [48] proposed a new WENO scheme smoothness indicator and analyzed its influence on the convergence to the steady-state solution. In 2011, Zhang et al. [47] proposed the WENO scheme to improve the convergence of the steady-state solutions of Euler equations. This new method had a good effect. But for several two-dimensional steady-state problems [47], there was still the phenomenon that the numerical residuals could not converge to machine zero. Wu et al. [42] designed a fixed-point sweeping WENO method to compute the steady-state hyperbolic conservation laws and discussed its convergence. It was found that the numerical residuals were difficult to approach machine zero for some examples.

At present, researchers have proposed many discontinuous Galerkin (DG) methods to compute the unsteady and steady-state problems. As early as 1973, Reed and Hill [36] innovatively proposed the first DG method in the study of neutron transport equations. The hybrid DG/FV methods [15, 16, 31, 45, 46] were designed for various problems. The application of a nonlinear limiter in the higher-order RKDG methods can effectively solve the problem of pseudo oscillation. Cockburn et al. [8–12] performed extensive research on the DG methods and applied the *minmod* type total variation bounded (TVB) limiters. Now many kinds of limiters have been developed, which are mainly divided into two categories: the slope-type limiters [2, 3, 5, 8–10, 12, 42] and the WENO limiters [1, 17, 18, 20, 25, 28–30, 32, 33]. The former can effectively solve the problem of pseudo oscillation, but the precision will decrease. When solving steady-state problems, both types have difficulties in the RKDG methods. Especially, when solving two-dimensional steady-state Euler equations on triangular meshes, the numerical residuals often can not converge to near machine zero.

It is found that when the third-order TVD Runge-Kutta method [40] and the classical finite difference WENO scheme [25, 39] are applied to simulate the steady-state problems, there is a problem that the numerical residual can not reduce to near machine zero. With further research, the scholars found that the new high-order WENO schemes [49] had a good performance. These methods can have the numerical residuals to converge close to machine zero, and there are no pseudo oscillations on structured or unstructured meshes. These new multi-resolution WENO schemes have a series of spatial templates with different sizes, which make the high-order accuracy schemes gradually reduce to the first-order accuracy near strong discontinuities. In this paper, the high-order RKDG methods with multi-resolution WENO limiters [50] are proposed for the first time to compute the steady-state problem on triangular meshes.

The rest parts of this paper are as follows. Section 2 introduces the RKDG methods to compute (2) on triangular meshes. For simulating two-dimensional steady-state problems on triangular meshes, a troubled cell indicator for unstructured meshes and high-order limiters are designed in Sect. 3. In Sect. 4, several steady-state problems are simulated to testify the effectiveness of the designed methods. The conclusions are described in Sect. 5.

### 2 RKDG Method on Triangular Meshes

Now we introduce the RKDG methods to compute (2) on triangular meshes. The DG methods have the numerical solutions on triangle cells  $\Delta_0$ . The test function space is  $V_h^k = \{v(x, y) : v(x, y)|_{\Delta_0} \in \mathbb{P}^k(\Delta_0)\}$ , where  $\mathbb{P}^k(\Delta_0)$  represents the set of polynomials with a total degree at most k on  $\Delta_0$ . We select the function  $u_h \in V_h^k$ , so that

$$\int_{\Delta_0} (u_h)_t v \, \mathrm{d}x \, \mathrm{d}y = \int_{\Delta_0} \left( f(u_h) v_x + g(u_h) v_y \right) \mathrm{d}x \, \mathrm{d}y - \int_{\partial \Delta_0} (f(u^h), g(u^h)) \cdot \mathbf{n} \, v \, \mathrm{d}s \tag{3}$$

for all test functions  $v \in V_h^k$ . The outward unit normal of the triangle boundary  $\partial \Delta_0$  is  $\mathbf{n} = (n_x, n_y)^{\mathrm{T}}$ .  $(f(u^h), g(u^h)) \cdot \mathbf{n}$  is an accurate or approximate Riemann solver in the system case, and is a monotone numerical flux in the scalar case. The third-order Runge-Kutta method [40]

$$\begin{cases} u^{(1)} = u^{n} + \Delta t L(u^{n}), \\ u^{(2)} = \frac{3}{4}u^{n} + \frac{1}{4}u^{(1)} + \frac{1}{4}\Delta t L(u^{(1)}), \\ u^{n+1} = \frac{1}{3}u^{n} + \frac{2}{3}u^{(2)} + \frac{2}{3}\Delta t L(u^{(2)}) \end{cases}$$
(4)

is used to design a fully discrete scheme.

## 3 Multi-resolution WENO Limiter

This section briefly describes the construction process of the troubled cell indicator which is extended from structured meshes [51] to unstructured meshes and high-order multi-resolution WENO limiters [50] on triangular meshes.

#### 3.1 Troubled Cell Indicator on Triangular Meshes

The objective is to identify the troubled cells on triangular meshes. If the number of troubled cells is too large, the computational cost will increase. But if the number is too small, the pseudo oscillation will occur. There have been a lot of discussions on the indicators of different troubled cells [35]. The troubled cell indicator in this paper is a generalization of the one in [51] to triangular meshes. Referring to Fig. 1,  $\Delta_{\ell}$ ,  $\ell = 1, 2, 3$  represent the adjacent triangular cells of  $\Delta_0$ .  $u_h(x, y, t)$  is the numerical solution of the indicator variable.

If it satisfies

$$\frac{\max_{\ell=1,2,3} \left( \left| \frac{1}{|\triangle_0|} \int_{\triangle_0} u_h(x,y,t) \right|_{\triangle_0} dx dy - \frac{1}{|\triangle_\ell|} \int_{\triangle_\ell} u_h(x,y,t) \left|_{\triangle_\ell} dx dy \right| \right)}{h_0 \min_{\ell=0,1,2,3} \left( \left| \frac{1}{|\triangle_\ell|} \int_{\triangle_\ell} u_h(x,y,t) \right|_{\triangle_\ell} dx dy \right| \right)} \ge 1,$$
(5)

then  $\triangle_0$  is considered to be a troubled cell. Here  $h_0$  represents the radius of the inscribed circle of  $\triangle_0$ . We will demonstrate later that this troubled cell indicator is very effective in the calculation of steady-state problems on triangular meshes.

#### 3.2 Multi-resolution WENO Limiter

From now on,  $u_h(x, y, t)$  is written as  $u_h(x, y)$  for convenience, if it does not cause confusion. Let  $\Delta_0$  be the troubled cell determined by the troubled cell indicator. The construction process of multi-resolution WENO limiters [50] for the scalar case is briefly described in the following. We construct multiple polynomials of various degrees on  $\Delta_0$ . We adopt a local orthogonal basis over  $\Delta_0$ : { $v_l^{(0)}(x, y), l = 0, \dots, K; K = (k + 1)(k + 2)/2 - 1$ }:

**Fig. 1** Triangular cells  $\triangle_0$ ,  $\triangle_1$ ,  $\triangle_2$ , and  $\triangle_3$ 



$$\begin{split} v_0^{(0)}(x,y) &= 1, \\ v_1^{(0)}(x,y) &= \frac{x - x_0}{\sqrt{|\Delta_0|}}, \\ v_2^{(0)}(x,y) &= a_{21} \frac{x - x_0}{\sqrt{|\Delta_0|}} + \frac{y - y_0}{\sqrt{|\Delta_0|}} + a_{22}, \\ &\vdots \end{split}$$

where  $(x_0, y_0)$  and  $|\triangle_0|$  are the barycenter and the area of  $\triangle_0$ , respectively. Then, we solve a linear system to obtain the values of  $a_{\ell m}$  by the orthogonality property:

$$\frac{1}{\int_{\Delta_0} \left(v_i^{(0)}(x,y)\right)^2 dx dy} \int_{\Delta_0} v_i^{(0)}(x,y) v_j^{(0)}(x,y) dx dy = \delta_{ij}.$$
(6)

We design  $q_{\ell}(x, y), \ell = 0, \dots, k$ , which satisfy

$$\int_{\Delta_0} q_{\ell}(x, y) v_l^{(0)}(x, y) dx dy = \int_{\Delta_0} u_h(x, y) v_l^{(0)}(x, y) dx dy, \ l = 0, \cdots, \frac{(\ell+1)(\ell+2)}{2} - 1.$$
(7)

Then, we set  $p_{0,1}(x, y) = q_0(x, y)$ . According to [6, 26, 27], we get the polynomials

$$p_{\ell,\ell}(x,y) = \frac{1}{\gamma_{\ell,\ell}} q_\ell(x,y) - \frac{\gamma_{\ell-1,\ell}}{\gamma_{\ell,\ell}} p_{\ell-1,\ell}(x,y), \ \ell = 1, \cdots, k$$
(8)

with  $\gamma_{\ell-1,\ell} + \gamma_{\ell,\ell} = 1$  and  $\gamma_{\ell,\ell} \neq 0$ , together with the polynomials

$$p_{\ell,\ell+1}(x,y) = \omega_{\ell,\ell} p_{\ell,\ell}(x,y) + \omega_{\ell-1,\ell} p_{\ell-1,\ell}(x,y), \ell = 1, \cdots, k-1$$
(9)

with  $\omega_{\ell-1,\ell} + \omega_{\ell,\ell} = 1$ . Here,  $\gamma_{\ell-1,\ell}$  and  $\gamma_{\ell,\ell}$  represent the linear weights, and  $\omega_{\ell-1,\ell}$  and  $\omega_{\ell,\ell}$  represent the nonlinear weights. We compute the smoothness indicators  $\beta_{\ell,\ell_2}$ . The smoothness indicators [25, 39] are constructed as

$$\beta_{\ell,\ell_2} = \sum_{|\alpha|=1}^{\kappa} \int_{\Delta_0} \Delta_0^{|\alpha|-1} \left( \frac{\partial^{|\alpha|}}{\partial x^{\alpha_1} \partial y^{\alpha_2}} p_{\ell,\ell_2}(x,y) \right)^2 \mathrm{d}x\mathrm{d}y, \ \ell = \ell_2 - 1, \ell_2; \ \ell_2 = 1, 2, 3,$$
(10)

where  $\kappa = \ell$ ,  $\alpha = (\alpha_1, \alpha_2)$ , and  $|\alpha| = \alpha_1 + \alpha_2$ . Here  $\beta_{0,1}$  is constructed as specified in [50]. Following [4, 7], we define

$$\tau_{\ell_2} = \left(\beta_{\ell_2,\ell_2} - \beta_{\ell_2-1,\ell_2}\right)^2, \quad \ell_2 = 1, 2, 3.$$
(11)

The nonlinear weights are

$$\omega_{\ell_1,\ell_2} = \frac{\bar{\omega}_{\ell_1,\ell_2}}{\sum\limits_{\ell=1}^{\ell_2} \bar{\omega}_{\ell,\ell_2}}, \ \bar{\omega}_{\ell_1,\ell_2} = \gamma_{\ell_1,\ell_2} \left( 1 + \frac{\tau_{\ell_2}}{\varepsilon + \beta_{\ell_1,\ell_2}} \right), \ \ell_1 = \ell_2 - 1, \ell_2; \ \ell_2 = 1, 2, 3.$$
(12)

Here  $\varepsilon$  is set as  $10^{-6}$ . The final new polynomial is

$$p^{\text{new}}(x,y) = \sum_{\ell=\ell_2-1}^{\ell_2} \omega_{\ell,\ell_2} p_{\ell,\ell_2}(x,y), \quad \ell_2 = 1, 2, 3$$
(13)

for the second-order, third-order, and fourth-order approximations, respectively.

Then we write (2) as

$$u_t + f_x(u) + g_y(u) = \frac{\partial}{\partial t} \begin{pmatrix} \rho \\ \rho \mu \\ \rho \nu \\ E \end{pmatrix} + \frac{\partial}{\partial x} \begin{pmatrix} \rho \mu \\ \rho \mu^2 + p \\ \rho \mu \nu \\ \mu(E+p) \end{pmatrix} + \frac{\partial}{\partial y} \begin{pmatrix} \rho \nu \\ \rho \mu \nu \\ \rho \mu \nu \\ \rho \nu^2 + p \\ \nu(E+p) \end{pmatrix} = 0.$$
(14)

Here  $\rho$  is the density,  $\mu$  and  $\nu$  are the velocities in *x*-direction and *y*-direction, respectively, *E* is the total energy,  $\gamma = 1.4$ , and  $p = \frac{E}{\gamma-1} - \frac{1}{2}\rho(\mu^2 + \nu^2)$  is the pressure. Let the Jacobian be  $(f'(u), g'(u)) \cdot \mathbf{n}_i = f'(u)n_{ix} + g'(u)n_{iy}$ , where  $\mathbf{n}_i = (n_{ix}, n_{iy})^T$ , i = 1, 2, 3 are the outward unit normals of the edges of the target cell. The eigenvectors of the Jacobian matrix [52] are

$$L_{i} = \begin{pmatrix} \frac{B_{2} + (\mu n_{ix} + \nu n_{iy})/c}{2} & -\frac{B_{1}\mu + n_{ix}/c}{2} & -\frac{B_{1}\nu + n_{iy}/c}{2} & \frac{B_{1}}{2} \\ \frac{n_{iy}\mu - n_{ix}\nu}{1 - B_{2}} & -\frac{n_{iy}}{B_{1}\mu} & B_{1}\nu & -B_{1} \\ \frac{B_{2} - (\mu n_{ix} + \nu n_{iy})/c}{2} & -\frac{B_{1}\mu - n_{ix}/c}{2} & -\frac{B_{1}\nu - n_{iy}/c}{2} & \frac{B_{1}}{2} \end{pmatrix}$$
(15)

and

$$R_{i} = \begin{pmatrix} 1 & 0 & 1 & 1 \\ \mu - cn_{i_{x}} & -n_{i_{y}} & \mu & \mu + cn_{i_{x}} \\ \nu - cn_{i_{y}} & n_{i_{x}} & \nu & \nu + cn_{i_{y}} \\ H - c(\mu n_{i_{x}} + \nu n_{i_{y}}) & -n_{i_{y}}\mu + n_{i_{x}}\nu & \frac{\mu^{2} + \nu^{2}}{2} & H + c(\mu n_{i_{x}} + \nu n_{i_{y}}) \end{pmatrix}, i = 1, 2, 3, (16)$$

and  $B_1 = \frac{\gamma-1}{c^2}$ ,  $B_2 = \frac{B_1(\mu^2 + v^2)}{2}$ ,  $c = \sqrt{\gamma p/\rho}$ , and  $H = \frac{E+p}{\rho}$ . For the relevant polynomial vectors  $p_0$ ,  $p_1$ ,  $p_2$ , and  $p_3$  on the troubled cell  $\Delta_0$ , the construction process of the multi-resolution WENO limiters [50] for the system case is briefly described in the following. We firstly construct the new polynomial vectors  $p_i^{\text{new}}$ , i = 1, 2, 3, in each  $\mathbf{n}_i$ -direction of the normal directions of  $\partial \Delta_0$  by applying the multi-resolution WENO limiting and relevant Jacobian  $f'(u)n_{ix} + g'(u)n_{iy}$ , i = 1, 2, 3. Then, we project  $p_0$ ,  $p_1$ ,  $p_2$ , and  $p_3$  into  $\tilde{p}_{i_l} = L_i \cdot p_l$ , i = 1, 2, 3, l = 0, 1, 2, 3.  $\tilde{p}_{i_l}$  is a 4-component vector, and every constituent is a polynomial to the degree k. For every constituent of  $\tilde{p}_{i_l}$ , we execute the scalar case of the multi-resolution WENO limiting procedure and get the 4-component vectors on  $\Delta_0$  as  $\tilde{p}_i^{\text{new}}$ , i = 1, 2, 3, respectively. Then we project  $\tilde{p}_i^{\text{new}}$  into the physical space  $p_i^{\text{new}} = R_i \cdot \tilde{p}_i^{\text{new}}$ , i = 1, 2, 3. Finally, the ultimate 4-component vector on  $\Delta_0$  is

$$p^{\text{new}} = \frac{\sum_{i=1}^{3} p_i^{\text{new}} |\Delta_i|}{\sum_{i=1}^{3} |\Delta_i|}.$$
 (17)

## **4** Numerical Results

Now, several steady-state problems are applied to testify the effectiveness of the secondorder, third-order, and fourth-order RKDG methods with multi-resolution WENO limiters (termed as the RKDG2-MRWENO, RKDG3-MRWENO, and RKDG4-MRWENO methods, respectively) on triangular meshes. For the two two-dimensional accuracy examples, the refinement is performed by a structured refinement, and all triangular cells are noted as the troubled cells, to verify that the accuracy, as well as the steady state convergence, is not affected even if the limiter is over-used in all cells. For the other examples, (5) is used to detect the troubled cells. For the RKDG2-MRWENO, RKDG3-MRWENO, and RKDG4-MRWENO methods, the CFL numbers are 0.3, 0.18, and 0.1, respectively. The numerical residual is given by

$$\operatorname{Res}_{A} = \sum_{i=1}^{N} \frac{|R1_{i}| + |R2_{i}| + |R3_{i}| + |R4_{i}|}{4 \times N},$$
(18)

in which  $R1_i = \frac{\partial \rho}{\partial t}|_i \approx \frac{\rho_i^{n+1} - \rho_i^n}{\Delta t}$ ,  $R2_i = \frac{\partial(\rho\mu)}{\partial t}|_i \approx \frac{(\rho\mu)_i^{n+1} - (\rho\mu)_i^n}{\Delta t}$ ,  $R3_i = \frac{\partial(\rho\nu)}{\partial t}|_i \approx \frac{(\rho\nu)_i^{n+1} - (\rho\nu)_i^n}{\Delta t}$ , and  $R4_i = \frac{\partial E}{\partial t}|_i \approx \frac{E_i^{n+1} - E_i^n}{\Delta t}$ . *N* is the total number of all triangular cells inside the computational field. The linear weights are set as  $\gamma_{\ell-1,\ell} = 0.01$  and  $\gamma_{\ell,\ell} = 0.99$ ,  $\ell = 1, 2, 3$ , respectively.

**Example 1** We compute the two-dimensional Euler equation (14). The calculation range is  $(x, y) \in [0, 2] \times [0, 2]$ .  $\rho(x, y, \infty) = 1 + 0.2 \sin(x - y)$ ,  $\mu(x, y, \infty) = 1$ ,  $\nu(x, y, \infty) = 1$ , and  $p(x, y, \infty) = 1$  are exact steady-state solutions. Figure 2 shows a sample mesh. The numerical residual is demonstrated in Fig. 3, in which the numerical residual is reduced to the minimum value of machine zero. The numerical errors and orders for the density at steady state are shown in Table 1. It is seen that the RKDG2-MRWENO, RKDG3-MRWENO, and RKDG4-MRWENO methods are performing well for this steady-state test case: the





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Fig. 3 Two-dimensional Euler equations for the steady-state problem. Case (1). Left: RKDG2-MRWENO method; middle: RKDG3-MRWENO method; right: RKDG4-MRWENO method. Diverse numbers represent different mesh levels of boundary points uniformly distributed from  $\frac{2}{5}$  to  $\frac{2}{80}$ 

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Table 1 Two-dimensional Euler equations for the steady-state problem. Case (1). $L^1$ - and $L^\infty$ -errors for density	RKDG2-J	RKDG2-MRWENO method				
	$     h     \frac{2}{5}     \frac{2}{10}     \frac{2}{20}     \frac{2}{40}     \frac{2}{52}     $	$L^1$ -error	Order	$L^{\infty}$ -error	Order	
		9.20E-4		4.08E-3		
		2.14E-4	2.10	1.05E-3	1.96	
		4.91E-5	2.13	2.44E-4	2.10	
		1.19E-5	2.05	6.33E-5	1.95	
		2.93E-6	2.02	1.61E-5	1.97	
	RKDG3-	RKDG3-MRWENO method				
	$ \frac{h}{2} = \frac{2}{5} = \frac{2}{10} = \frac{2}{20} = \frac{2}{20} = \frac{2}{80} =$	$L^1$ -error	Order	$L^{\infty}$ -error	Order	
		1.77E-4		7.24E-4		
		2.16E-5	3.03	1.19E-4	2.60	
		2.86E-6	2.92	1.68E-5	2.83	
		3.79E-7	2.92	2.26E-6	2.89	
		4.93E-8	2.94	2.92E-7	2.96	
		MRWENO method	l			
	h	$L^1$ -error	Order	$L^{\infty}$ -error	Order	
	$     \frac{2}{5}     \frac{2}{10}     \frac{2}{20}     \frac{2}{40}     \frac{2}{80}   $	1.91E-6		6.43E-6		
		1.13E-7	4.08	5.17E-7	3.64	
		5.73E-9	4.30	3.34E-8	3.95	
		3.16E-10	4.18	2.33E-9	3.84	
		1.99E-11	3.99	1.33E-10	4.13	

numerical residual settles to near machine zero, and the designed order of the accuracy is achieved.

**Example 2** The shock reflection problem. The calculation range is  $(x, y) \in [0, 4] \times [0, 1]$ . The Dirichlet conditions are applied on the other two sides



Fig. 4 The shock reflection problem. Sample mesh



**Fig.5** The shock reflection problem. Fifteen equally spaced density contours from 1.14 to 2.60. Top: RKDG2-MRWENO method; middle: RKDG3-MRWENO method; bottom: RKDG4-MRWENO method. Boundary points are  $h = \frac{1}{30}$ 

$$(\rho, \mu, \nu, p)^{\mathrm{T}} = \begin{cases} (1.0, 2.9, 0, 1.0/1.4)^{\mathrm{T}}|_{(0, y, t)^{\mathrm{T}}}, \\ (1.699\,97, 2.619\,34, -0.506\,32, 1.528\,19)^{\mathrm{T}}|_{(x, 1, t)^{\mathrm{T}}}. \end{cases}$$
(19)

Figure 4 shows a sample mesh. Figure 5 shows the density contours of 15 equidistant contours from 1.14 to 2.60. Figure 6 shows the troubled cells identified in the termination time. It is observed that the RKDG4-MRWENO method has better resolution than that of the RKDG2-MRWENO method and RKDG3-MRWENO method, especially for the accurate capture of strong shocks. The numerical residual is shown in Fig. 7. It is found that the average residual of the RKDG-MRWENO methods can reduce to about  $10^{-12}$ , near machine zero.



**Fig. 6** The shock reflection problem. The square represents the cells identified as troubled cells at the end of time. Top: RKDG2-MRWENO method; middle: RKDG3-MRWENO method; bottom: RKDG4-MRWENO method. Boundary points are  $h = \frac{1}{30}$ 



**Fig.7** The shock reflection problem. Left: RKDG2-MRWENO method; middle: RKDG3-MRWENO method; right: RKDG4-MRWENO method. Boundary points are  $h = \frac{1}{30}$ 

**Example 3** Two transonic steady-state problems of NACA0012 airfoil [38] with  $M_{\infty} = 0.8$ ,  $\alpha = 1.25^{\circ}$  and  $M_{\infty} = 0.85$ ,  $\alpha = 1^{\circ}$ . The calculation range is  $[-15, 15] \times [-15, 15]$ . Figure 8 shows a sample mesh. Thirty equally spaced pressure contours are shown in Figs. 9 and 10. We observe that the average residual of the RKDG-MRWENO methods can reduce to about  $10^{-12.5}$ , near machine zero via time advancing.



Fig. 8 NACA0012 airfoil sample mesh. Left: whole region; right: zoomed-in figure near the airfoil



**Fig.9** NACA0012 airfoil.  $M_{\infty} = 0.8$  and  $\alpha = 1.25^{\circ}$ . Top: 30 equally spaced pressure contours from 0.50 to 1.46; middle: troubled cells are mainly in [-3, 3] × [-3, 3]; bottom: the evolution of the average numerical residual. Left: RKDG2-MRWENO method; middle: RKDG3-MRWENO method; right: RKDG4-MRWENO method

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**Fig. 10** NACA0012 airfoil.  $M_{\infty} = 0.85$  and  $\alpha = 1^{\circ}$ . Top: 30 equally spaced pressure contours from 0.49 to 1.54; middle: troubled cells are mainly in [-3, 3] × [-3, 3]; bottom: the evolution of the average numerical residual. Left: RKDG2-MRWENO method; middle: RKDG3-MRWENO method; right: RKDG4-MRWENO method

**Example 4** Two supersonic steady-state problems of NACA0012 airfoil [38] with  $M_{\infty} = 2$ ,  $\alpha = 1^{\circ}$  and  $M_{\infty} = 3$ ,  $\alpha = 1.5^{\circ}$ . Figure 8 is also a computational mesh for this example. Thirty equally spaced pressure contours are demonstrated in Figs. 11 and 12, respectively. It is again observed that the average residual of the RKDG-MRWENO methods can reduce to about  $10^{-12}$ , near machine zero.



**Fig. 11** NACA0012 airfoil.  $M_{\infty} = 2$  and  $\alpha = 1^{\circ}$ . Top: 30 equally spaced pressure contours from 0.76 to 5.35; middle: troubled cells are mainly in  $[-3, 7] \times [-5, 5]$ ; bottom: the evolution of the average numerical residual. Left: RKDG2-MRWENO method; middle: RKDG3-MRWENO method; right: RKDG4-MRWENO method



**Fig. 12** NACA0012 airfoil.  $M_{\infty} = 3$  and  $\alpha = 1.5^{\circ}$ . Top: 30 equally spaced pressure contours from 0.76 to 11.35; middle: troubled cells are mainly in [-3, 7] × [-5, 5]; bottom: the evolution of the average numerical residual. Left: RKDG2-MRWENO method; middle: RKDG3-MRWENO method; right: RKDG4-MRWENO method

**Example 5** Two transonic steady-state problems of NACA001035 airfoil [14] with  $M_{\infty} = 0.8$ ,  $\alpha = 1.25^{\circ}$  and  $M_{\infty} = 0.9$ ,  $\alpha = 0.5^{\circ}$ . The calculation range is [-16, 16] × [-16, 16]. Figure 13 shows a sample mesh containing 5 593 triangles. Equally spaced pressure contours are demonstrated in Figs. 14 and 15. It is found that the residual of the RKDG-MRWENO methods can reduce to about  $10^{-14.5}$ , near machine zero.



Fig. 13 NACA001035 airfoil sample mesh. Left: whole region; right: zoomed-in figure near the airfoil



**Fig. 14** NACA001035 airfoil.  $M_{\infty} = 0.8$  and  $\alpha = 1.25^{\circ}$ . Top: 30 equally spaced pressure contours from 0.67 to 1.43; middle: troubled cells are mainly in [-3, 3] × [-3, 3]; bottom: the evolution of the average numerical residual. Left: RKDG2-MRWENO method; middle: RKDG3-MRWENO method; right: RKDG4-MRWENO method

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**Fig. 15** NACA001035 airfoil.  $M_{\infty} = 0.9$  and  $\alpha = 0.5^{\circ}$ . Top: 30 equally spaced pressure contours from 0.46 to 1.58; middle: troubled cells are mainly in [-3, 3] × [-3, 3]; bottom: the evolution of the average numerical residual. Left: RKDG2-MRWENO method; middle: RKDG3-MRWENO method; right: RKDG4-MRWENO method

**Example 6** Two supersonic steady-state problems of NACA001035 airfoil [14] with  $M_{\infty} = 1.5$ ,  $\alpha = 1.5^{\circ}$  and  $M_{\infty} = 2$ ,  $\alpha = 1^{\circ}$ . The calculation range is  $[-16, 16] \times [-16, 16]$ . Figure 13 is also a sample mesh containing 5 593 triangles for this example. Equally spaced pressure contours are shown in Figs. 16 and 17. It is found that the average residual of the RKDG-MRWENO methods can reduce to about  $10^{-14}$ , near machine zero.



**Fig. 16** NACA001035 airfoil.  $M_{\infty} = 1.5$  and  $\alpha = 1.5^{\circ}$ . Top: 30 equally spaced pressure contours from 0.51 to 3.21; middle: troubled cells are mainly in [-3, 7] × [-5, 5]; bottom: the evolution of the average numerical residual. Left: RKDG2-MRWENO method; middle: RKDG3-MRWENO method; right: RKDG4-MRWENO method



**Fig. 17** NACA001035 airfoil.  $M_{\infty} = 2$  and  $\alpha = 1^{\circ}$ . Top: 60 equally spaced pressure contours from 0.54 to 5.15; middle: troubled cells are mainly in [-3, 7] × [-5, 5]; bottom: the evolution of the average numerical residual. Left: RKDG2-MRWENO method; middle: RKDG3-MRWENO method; right: RKDG4-MRWENO method

**Example 7** Two transonic steady-state problems of CAST7 airfoil [14] with  $M_{\infty} = 0.8$ ,  $\alpha = 1.25^{\circ}$  and  $M_{\infty} = 0.85$ ,  $\alpha = 1^{\circ}$ . The calculation range is  $[-16, 16] \times [-16, 16]$ . Figure 18 shows a sample mesh containing 5 593 triangles. Equally spaced pressure contours are shown in Figs. 19 and 20. It is observed that the average residual of the RKDG-MRWENO methods can reduce to about  $10^{-14.5}$ , near machine zero once again.



Fig. 18 CAST7 airfoil sample mesh. Left: whole region; right: zoomed-in figure near the airfoil



**Fig. 19** CAST7 airfoil.  $M_{\infty} = 0.8$  and  $\alpha = 1.25^{\circ}$ . Top: 30 equally spaced pressure contours from 0.41 to 1.46; middle: troubled cells are mainly in  $[-3, 3] \times [-3, 3]$ ; bottom: the evolution of the average numerical residual. Left: RKDG2-MRWENO method; middle: RKDG3-MRWENO method; right: RKDG4-MRWENO method



**Fig. 20** CAST7 airfoil.  $M_{\infty} = 0.85$  and  $\alpha = 1^{\circ}$ . Top: 30 equally spaced pressure contours from 0.42 to 1.53; middle: troubled cells are mainly in  $[-3, 3] \times [-3, 3]$ ; bottom: the evolution of the average numerical residual. Left: RKDG2-MRWENO method; middle: RKDG3-MRWENO method; right: RKDG4-MRWENO method

**Example 8** Two supersonic steady-state problems of CAST7 airfoil [14] with  $M_{\infty} = 2$ ,  $\alpha = 1^{\circ}$  and  $M_{\infty} = 2$ ,  $\alpha = 2^{\circ}$ . The calculation range is  $[-16, 16] \times [-16, 16]$ . Figure 18 is also the sample mesh containing 5 593 triangles for this example. Equally spaced pressure contours are shown in Figs. 21 and 22. It is observed that the average residual of the RKDG-MRWENO methods can reduce to about  $10^{-14}$ , near machine zero once again.



**Fig. 21** CAST7 airfoil.  $M_{\infty} = 2$  and  $\alpha = 1^{\circ}$ . Top: 60 equally spaced pressure contours from 0.65 to 5.17; middle: troubled cells are mainly in  $[-3, 7] \times [-5, 5]$ ; bottom: the evolution of the average numerical residual. Left: RKDG2-MRWENO method; middle: RKDG3-MRWENO method; right: RKDG4-MRWENO method



**Fig. 22** CAST7 airfoil.  $M_{\infty} = 2$  and  $\alpha = 2^{\circ}$ . Top: 60 equally spaced pressure contours from 0.62 to 5.24; middle: troubled cells are mainly in [-3, 7] × [-5, 5]; bottom: the evolution of the average numerical residual. Left: RKDG2-MRWENO method; middle: RKDG3-MRWENO method; right: RKDG4-MRWENO method

# 5 Conclusions

In this article, a troubled cell indicator for unstructured meshes is designed and highorder multi-resolution WENO schemes [50] are served as limiters for the RKDG methods to simulate steady-state problems on triangular meshes. The main objective is to apply the modified troubled cell indicator to detect troubled cells subject to the multiresolution WENO limiting procedure, and construct a sequence of hierarchical  $L^2$  projection polynomial solutions of the DG methods over triangular troubled cell itself. Using the second-order, third-order, and fourth-order RKDG-MRWENO methods, the spurious oscillations can be well suppressed and the average residual can reduce to near machine zero. Extensive examples are applied to verify that such high-order RKDG-MRWENO methods have good effectiveness when calculating steady-state problems. **Funding** Jun Zhu: Research is supported by the NSFC Grant No. 11872210 and Grant No. MCMS-I-0120G01. Chi-Wang Shu: Research is supported by the AFOSR Grant FA9550-20-1-0055 and the NSF Grant DMS-2010107. Jianxian Qiu: Research is supported by the NSFC Grant No. 12071392.

# **Compliance with Ethical Standards**

**Conflict of Interest** On behalf of all authors, the corresponding author states that there is no conflict of interest.

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